

# POLarization-diversity Doppler Radars On Satellites (POLYDOROS)

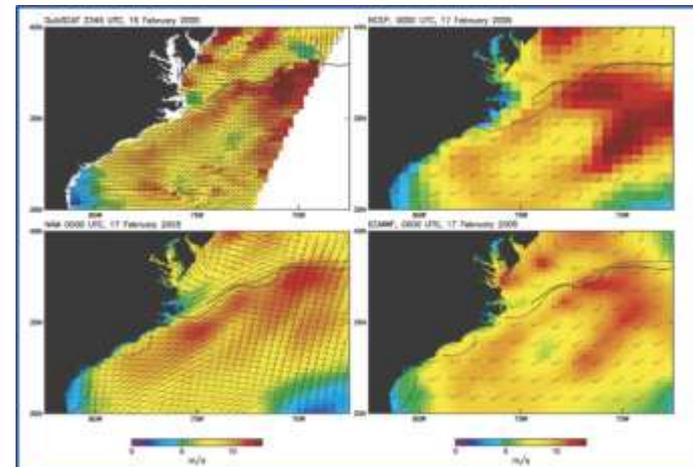
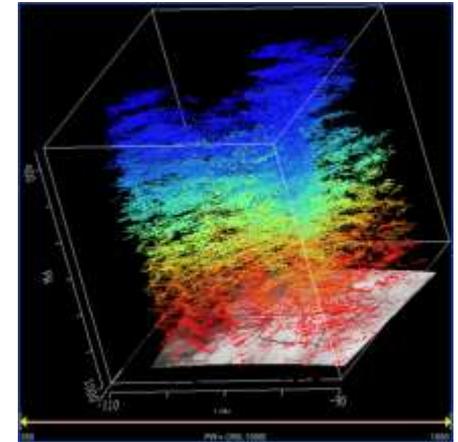
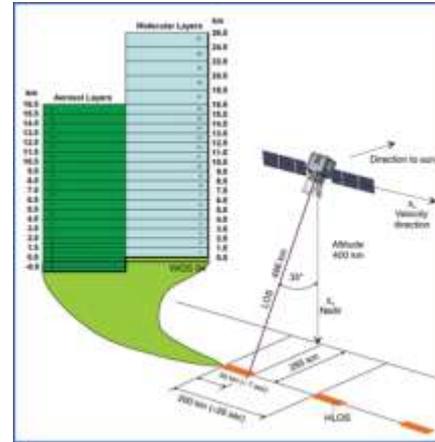
## *Principal Investigators:*

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- Alessandro Battaglia (University of Leicester, UK)

Presented by N. Humpage

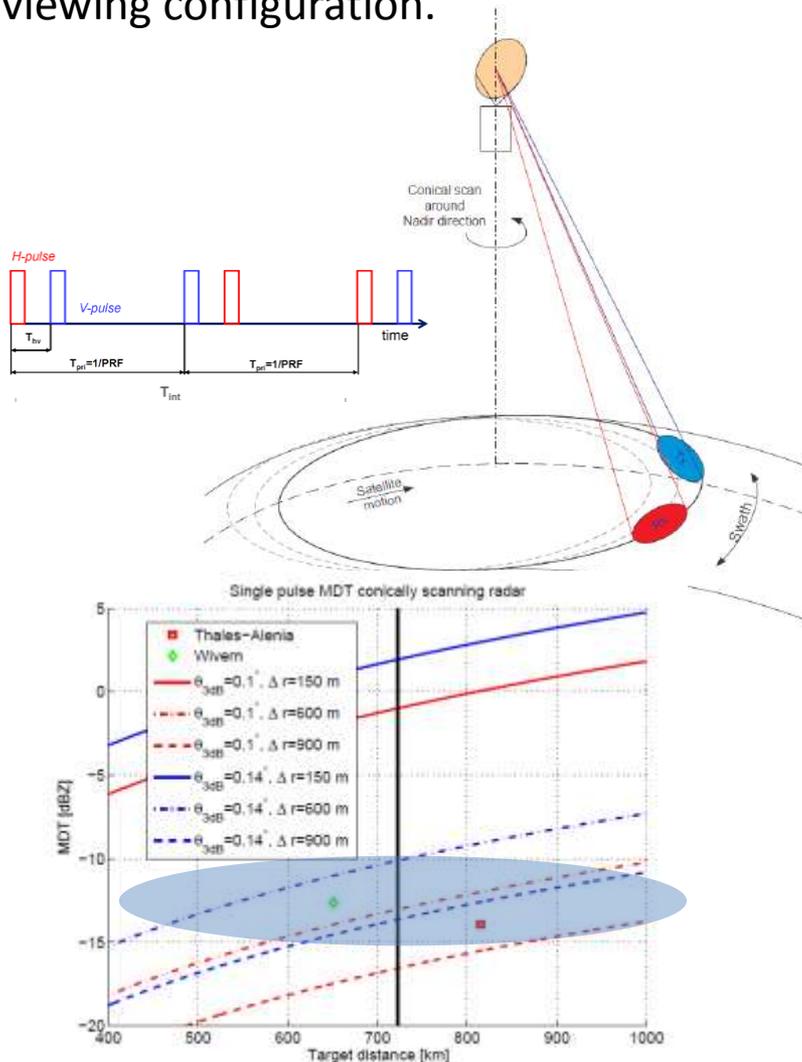
# Requirement for wind field observations

- Three user communities with requirement for improved wind field observations (particularly spatial and temporal coverage):
  - NWP and data assimilation
  - Hurricanes
  - Cloud modelling
- Current/proposed observation techniques:
  - **ADM-Aeolus**: Doppler lidar, provides global coverage but low frequency of observation, unable to observe within clouds
  - **Visible/IR (spectral) imaging from GEO, e.g. from GOES**: infer wind speeds from movement of clouds in successive images (every 7.5 minutes), altitude determination is problematic... spectral imaging (e.g. from MTG-IRS) would improve this whilst maintaining high frequency of observation and good spatial resolution, albeit over only one portion of the globe
  - **Scatterometers, e.g. QuikSCAT**: active radar (14 GHz) technique measures wind speeds just above the ocean surface under clear and cloudy conditions



# Conically scanning W-band radar

Different conically scanning W-band polarization diversity radars concepts have been previously studied by ESA (Thales-Alenia and Wivern study). Only slight differences in viewing configuration.



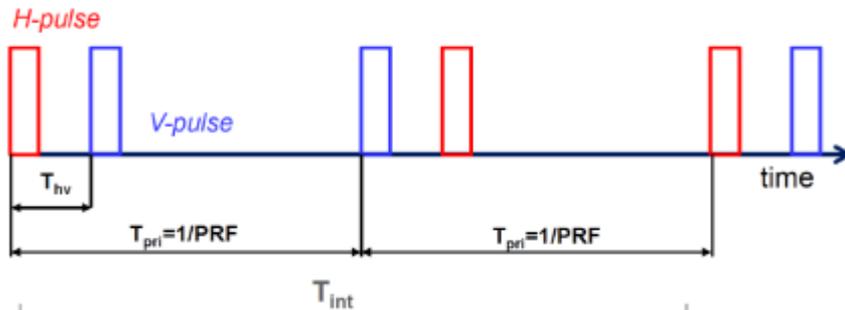
Frequency	94 GHz
Peak power	1 kW
Satellite height	550(500 – 600) km ( $v_{sat} = 7.7 \text{ km s}^{-1}$ )
Incidence angle	42.5[41.7° – 45°](scanning angle = 38.5[37.8 – 40.2]°)
Swath	900(800 – 1050) km
Distance from ground	723(651 – 815) km
Antenna rotation velocity	8.6/13 RPM Footprint velocity 354/612.3 km/s
Antenna diameter	1.59 – 2.23 m ( $\theta_{3dB} = 0.14^\circ – 0.1^\circ$ )
Antenna side lobes	< 30 dB
Pulse-length	3 – 6 $\mu\text{sec}$ ( $\Delta r = 450 – 900\text{m}$ )
Pair separation	$TBD(V_{Nyq}$ accordingly)
$PRF_{pairs}$	3000-3600Hz [50-41.6 km slant-range ambiguity]
Total system losses	6dB
Integration time	$TBD$
Receiver bandwidth	according to pulse-length
Noise figure	6.5 dB

In this project: 1) in-depth **error budget study**  
 2) Advantage of adding **pulse compression**

# Error budget

Doppler measurements are affected by a variety of errors, ranging from noise to multiple scattering, non uniform beam filling, aliasing, and pointing errors.

$$\epsilon_{TOT}^2 = \epsilon_N^2 + \epsilon_{NUBF}^2 + \epsilon_{aliasing}^2 + \epsilon_{MS}^2 + \epsilon_{pointing}^2 \quad \text{Total quadratic error}$$

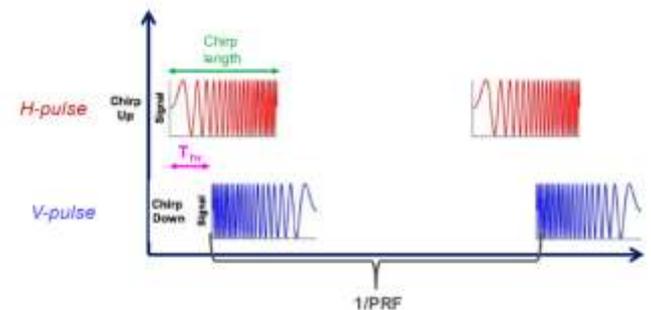


PD ensures that we get rid of aliasing!

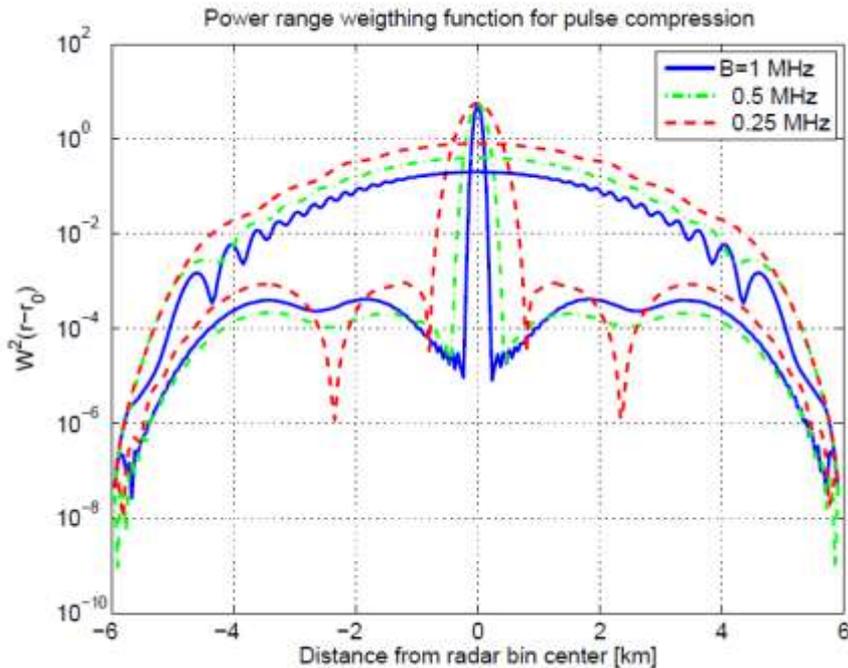
$$T_{hv} = 5 \mu\text{sec} \rightarrow v_{Ny} = 160 \text{ m/s}$$

$$T_{hv} = 20 \mu\text{sec} \rightarrow v_{Ny} = 40 \text{ m/s} \quad (\text{no aliasing for wind up to } 203 \text{ km/h})$$

But cross-talk introduced by multiple scattering, depolarizing atmospheric targets, ground clutter, instrument cross talk must be reduced  $\rightarrow$  V and H signal transmitted with opposite slopes

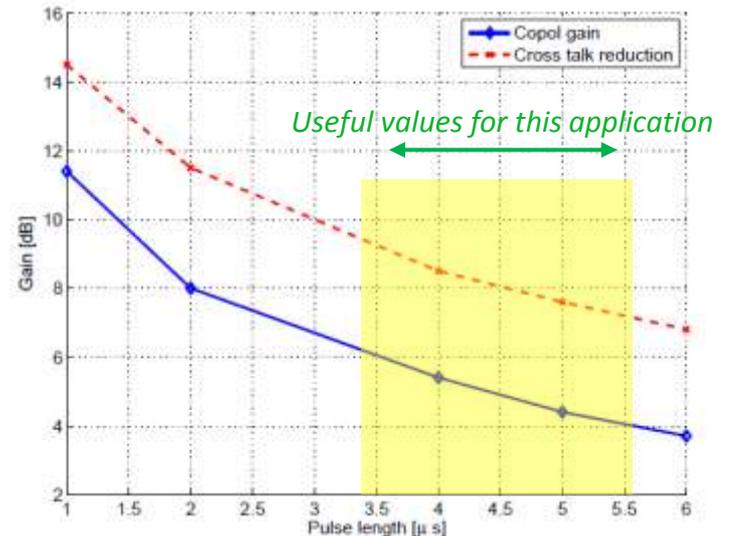


# Range sidelobes for pulse compression

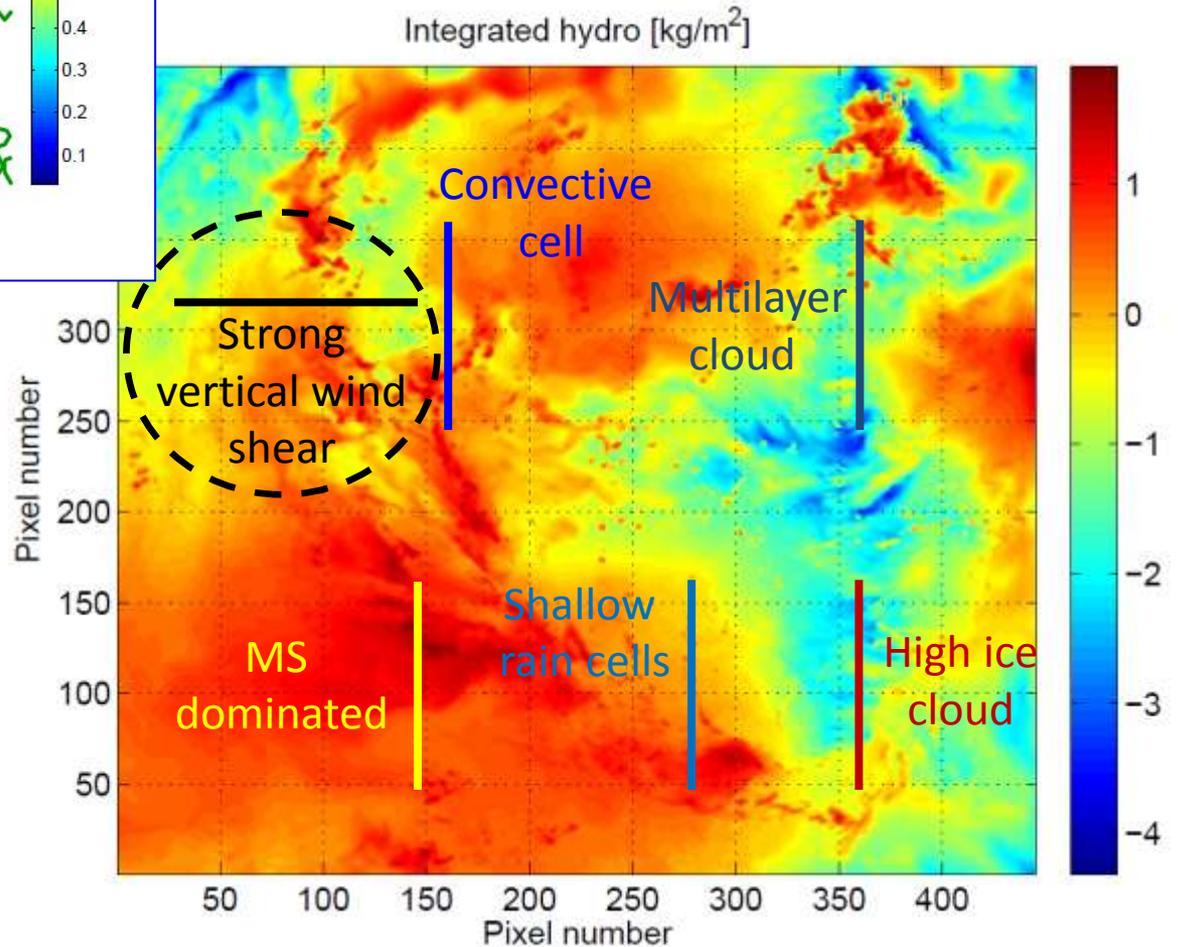
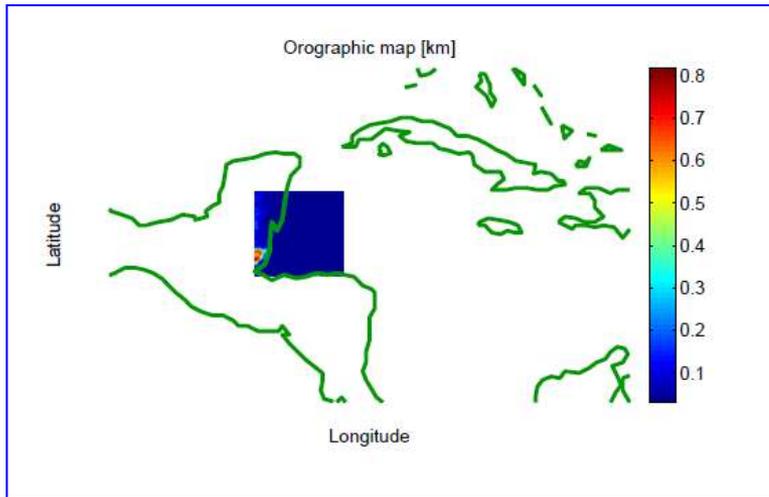


Surface type	Cross section	Range sidelobe level
Land, typical	-10 dB	-39 dB
Land, worst case	-5 dB	-44 dB
Sea, typical	-15 dB	-34 dB
Sea, worst case	-10 dB	-39 dB
Snow, typical	0 dB	-49 dB
Snow, worst case	3 dB	-52 dB

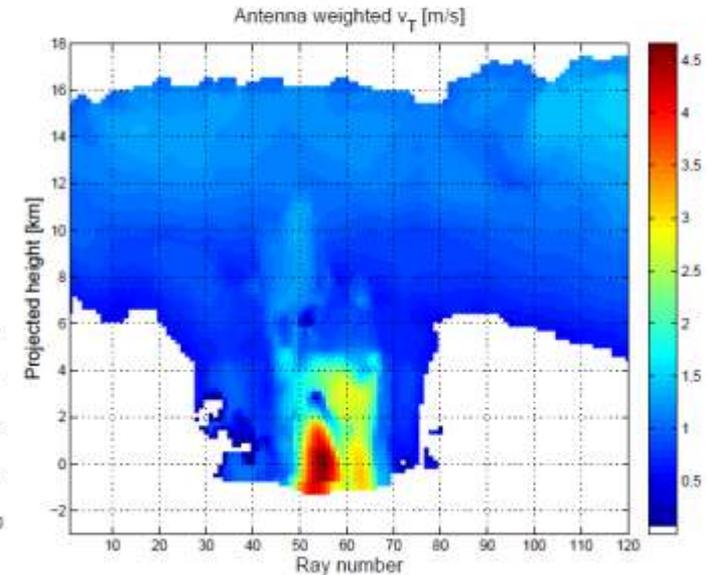
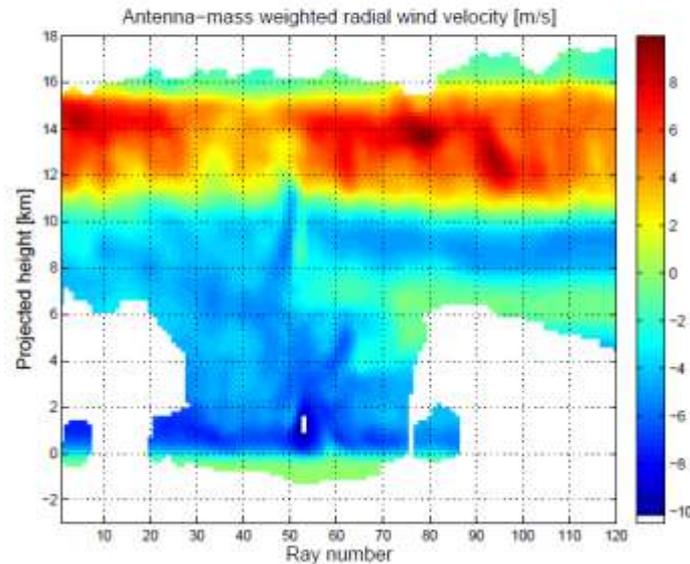
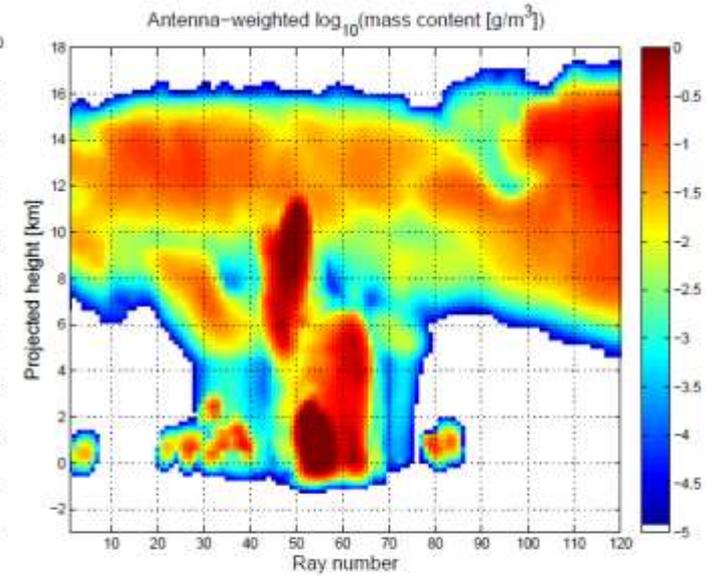
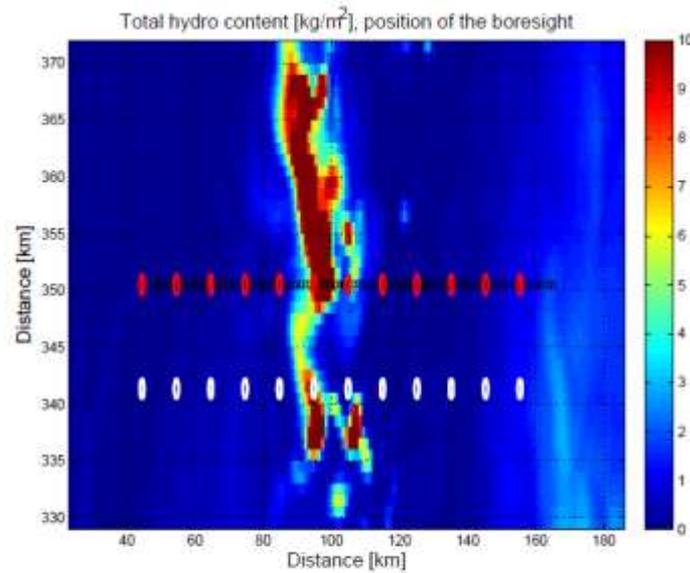
Pulse compression with sidelobe suppression approaching 40 (50) dB for a 0.25 (1) MHz chirp bandwidth can be achieved. This is adequate for this application, especially over sea surfaces characterized by very low  $\sigma_0$ . The 2 chirp mode offers some improvement in Doppler accuracy by reducing crosstalk between H and V-polarized channels



# Hurricane Karl simulation

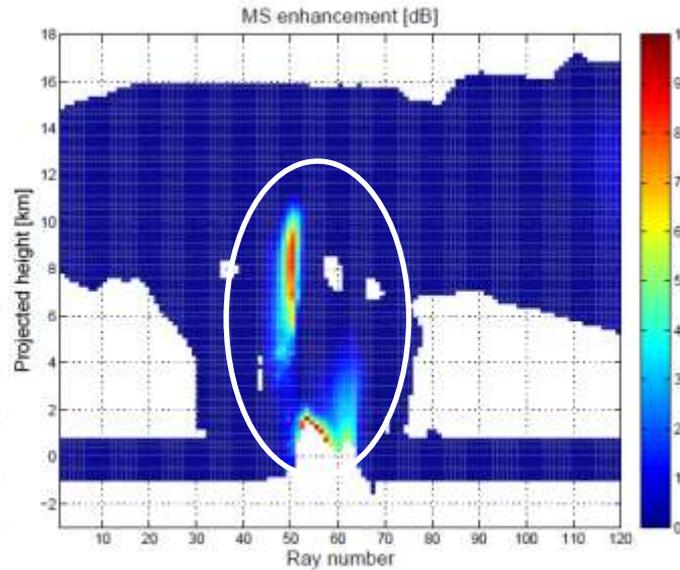
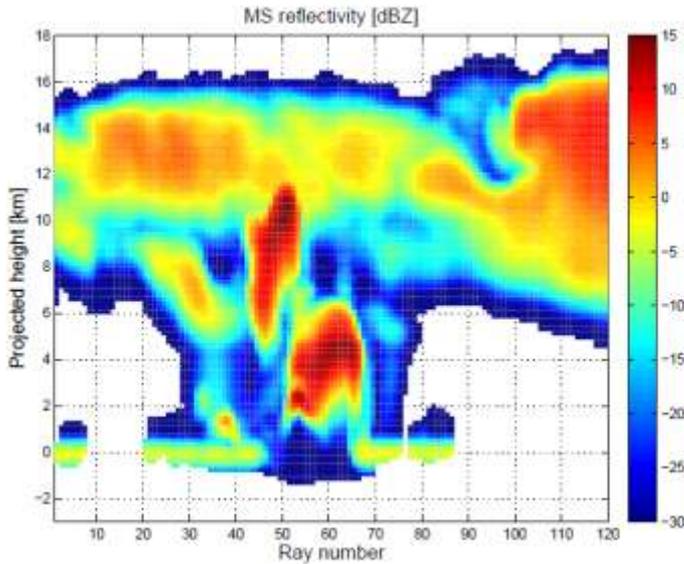


# Forward view: strong vertical wind shear



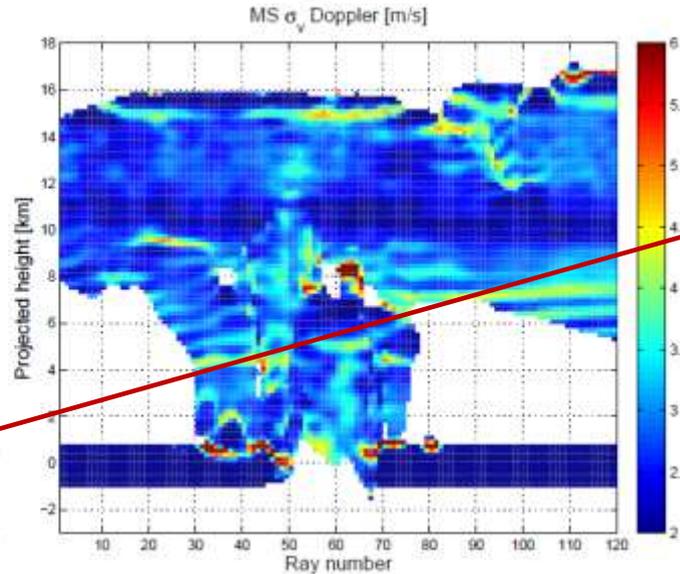
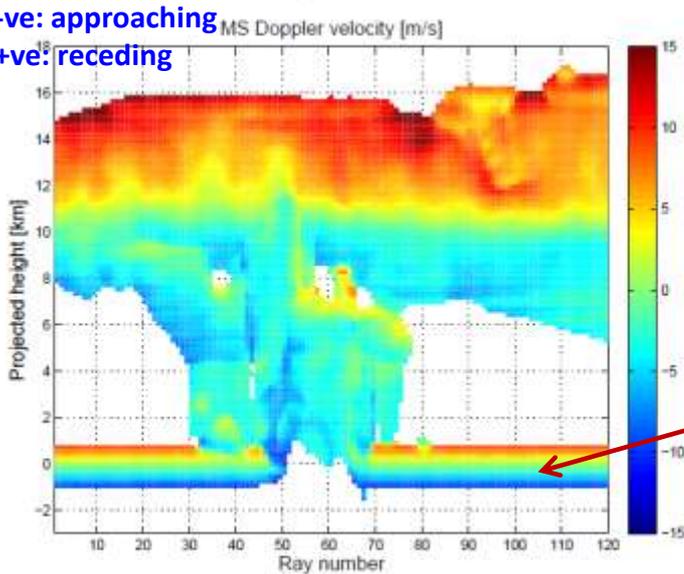
-ve: approaching  
+ve: receding

# Forward modelling



MS effects is relevant in convective cores: in such regions it tend to produce errors of the order of 1-2 m/s even when averaging at 10 km distance (convective scale).

-ve: approaching  
+ve: receding

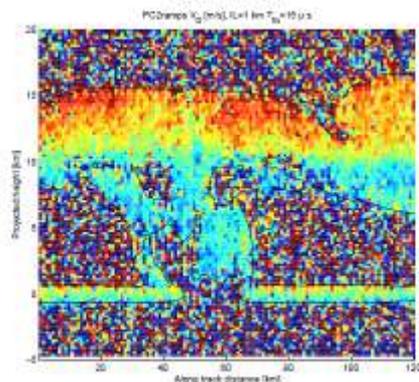
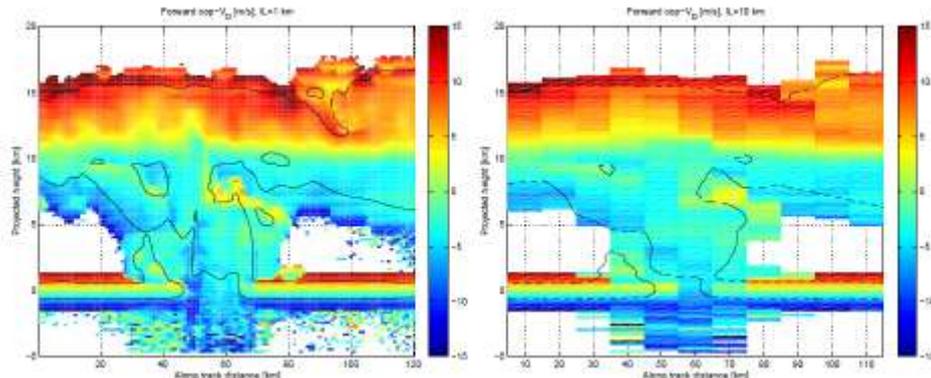


At forward view surface appears to have  $V_D \neq 0$

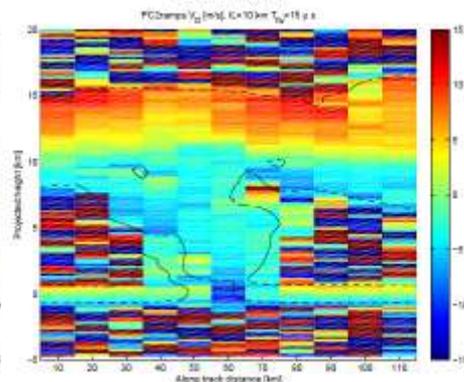
Spectral widths = 3 to 3.5 m/s (smaller than at side view)

When first seen at projected height > 0 the surface appears moving downward

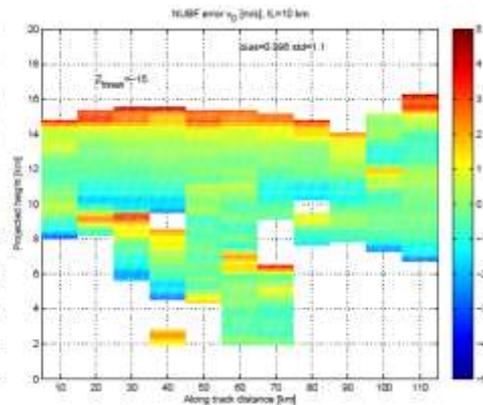
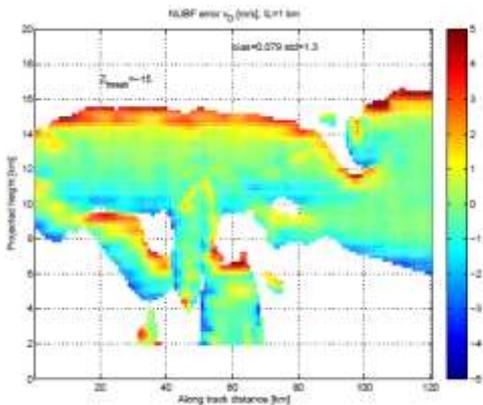
# Noise and NUBF error at 1 and 10 km integration



$\epsilon_N = 3.6 \text{ m/s}$



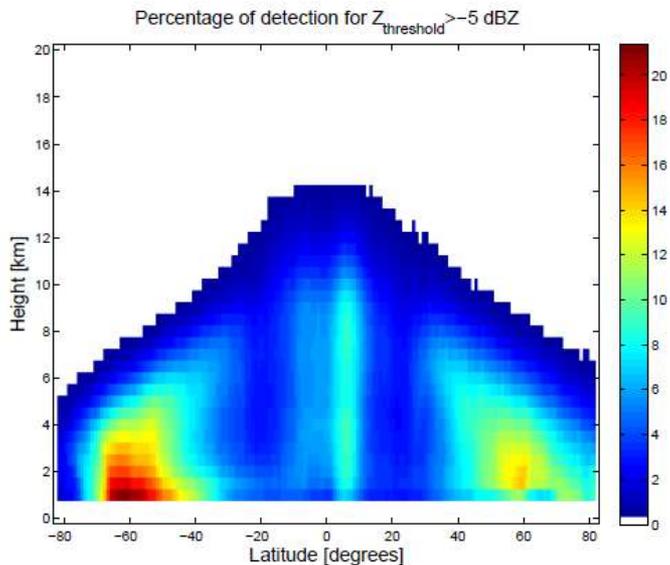
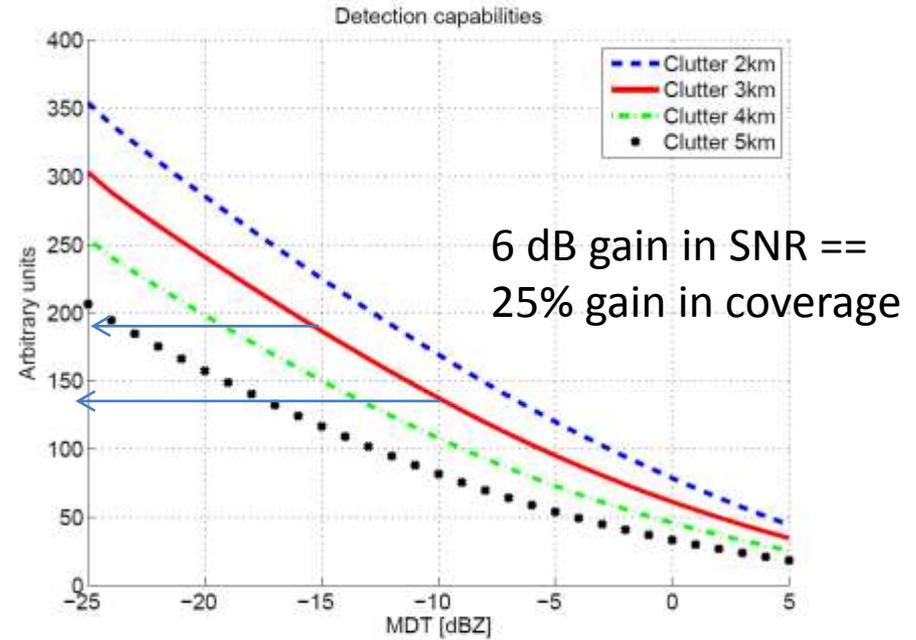
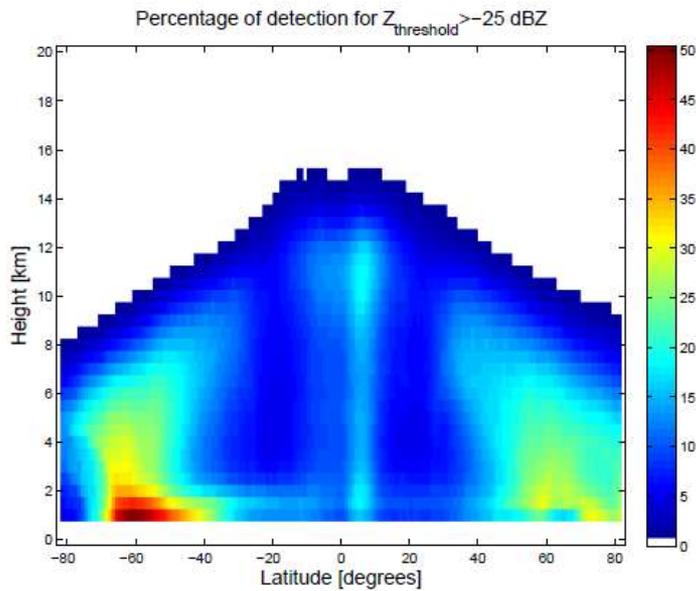
$\epsilon_N = 0.8 \text{ m/s}$



The vertical shear is well captured!  
 There is a significant reduction of  $\epsilon_N$  (typically below 1 m/s) when averaging for 10 km (with optimal  $T_{hv}$  around 10-20  $\mu\text{s}$ ).

*NUBF* seems to be the main driver of errors with increasingly importance when moving towards the forward/backward section of the scan. Since clouds are horizontally stratified averaging along footprint track is not mitigating the problem. Biases up to 3 m/s are expected in correspondence of regions with vertical reflectivity inhomogeneity.

# Gain in coverage (based on CloudSat)



These figures assess the degradation in detection for a radar system with lower sensitivity and higher clutter height than those achieved for the CloudSat radar. Roughly speaking passing from an  $MDT$  value of  $-25$  dBZ to  $MDT$  equal  $5$  dBZ reduces the detection capability by a factor of 8 to 11 (with clutter height ranging between 2 and 5 km).

# Conclusions

- Obvious **benefit for larger antenna size** (but less coverage)
- **NUBF seems to be the main driver of errors** (bottleneck) with increasingly important effect going towards forward/backward viewing directions and with increasing sensitivity. There are no strategies in place to correct for it! **Averaging along footprint track is not a panacea**
- **Noise errors can be brought down to less than 1-1.5m/s for 10 km integration** (even for the 13 RPM system) for signal above -10 dBZ (preliminary analysis show that this corresponds to  $\sim 40\%$  of CloudSat detection)
- Pulse compression works fine with peak to sidelobe of  $\sim 40$  dB (but only ocean surfaces considered up to now).
- 2-chirp mode. Not essential but the benefit may increase in presence of larger depolarization effects (e.g. brighter surfaces/MS cells).

***Pulse compression is a plausible option for a conically scanning W-band polarization diversity radar system. The key advantage of such systems is the low reflectivity of ocean surfaces at slant incidence angles, which poses less stringent constraints onto range side-lobe suppression. A system with a bandwidth of 0.25 MHz, with a chirp length of 40  $\mu$ s and with  $T_{hv}$  in the range between 10 and 20  $\mu$ s provides a good balance between vertical resolution, Doppler accuracy and coverage. We expect that such system will provide useful Doppler (accuracies better than 2 m/s) at 1 km vertical resolution and 10km integration on roughly half of the cloudy regions as detected by CloudSat.***